

#### Statistical Modeling of Repairable Systems



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### Overview

- Review of standard process models assumptions/shortcomings
- Describe modulated process model
- Introduce statistical inference procedures
- > Overview of simulation results
- > Derivation for probability of mission success
- > Summary



#### **Common Process Models**

- Models for repairable systems must be able to describe the occurrence of events in time, and are thus inherently different from models nonrepairable systems.
- Renewal Process: (good as new) A repaired unit is always brought to a like-new condition – time between failures are independent and identically distributed (iid). For this reason, the renewal process cannot be used to model a system experiencing deterioration or reliability improvement. (examples: Gamma).
- ➤ Non-homogeneous Poisson Process (NHPP): (same as old)
  Following the repair, the system is returned to the state just prior to failure. (examples: Weibull / Power Law)
- In practice, neither process seems realistic. In many cases, a repaired unit is in better condition than it was just before failure, but still not in a like-new condition

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#### **Modulated Process**

- Inhomogeneous gamma process (Berman 1981): Suppose that events, or shocks, occur according to an NHPP with intensity function u(t), and suppose that a failure occurs not every shock but at every Kappa(th) shock, where Kappa is a positive integer.
- > The joint probability density function for the first n failures is given by

$$f(t_1, t_2, ..., t_n) = \left\{ \prod_{i=1}^n u(t_i) [U(t_i) - U(t_{i-1})]^{k-1} \right\} \times \frac{exp[-U(t_i)]}{[G(k)]^n}$$

• U(t) is the expected number of shocks before time t and is defined as

$$U(t) = \int_0^t u(x) \ dx.$$







- $\succ$  If for example Kappa  $(m{k})$  equaled 4, then every fourth shock would cause a failure
- A failed and repaired unit would be better than it was just before failure, since in order to cause another failure the required improvement parameter (Kappa) must accumulate to four again. A failed and repaired unit would not necessarily be as good as new.

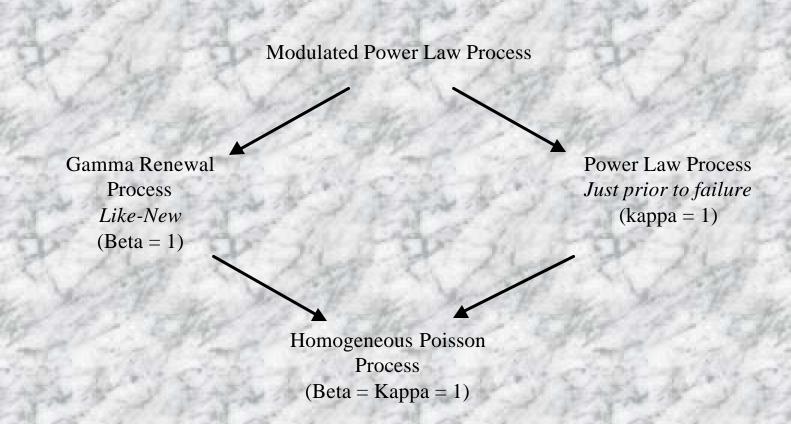
#### > Parameter definitions

- > Kappa: measure if the improvement effected by the repair
- > Beta: is a measure of the system improvement or deterioration over the course of a systems life
- Theta: Scaling parameter (units)



## Modulated Power Law Process (Special Cases)

There are three special cases of the Modulated Power Law Process







## Modulated Power Law Process Point Estimation

If we take partial derivatives of the likelihood function with respect to theta,beta, and kappa we obtain the likelihood equations

$$l(\boldsymbol{q}, \boldsymbol{b}, \boldsymbol{k}) = -\left(\frac{t_n}{\boldsymbol{q}}\right)^{\boldsymbol{b}} + n\ln(\boldsymbol{b}) - n\ln(\Gamma(\boldsymbol{k})) - n\boldsymbol{b}\boldsymbol{k}\ln\boldsymbol{q} + (\boldsymbol{b} - 1)\sum_{i=1}^{n}\ln t_i + (\boldsymbol{k} - 1)\sum_{i=1}^{n}\ln(t_i^{\boldsymbol{b}} - t_{i-1}^{\boldsymbol{b}})$$

$$\frac{\partial l}{\partial \boldsymbol{q}} = \left[\left(\frac{\text{Beta}}{\text{Theta}}\right)\left(\frac{t_n}{\text{Theta}}\right)^{\text{Beta}}\right] - \left[\frac{(n \cdot \text{Beta} \cdot \text{Kappa})}{\text{Theta}}\right] = 0$$

$$\frac{\partial l}{\partial \boldsymbol{b}} = -\left[\left(\frac{t_{n}}{Theta}\right)^{Beta} \cdot \left(\ln\left(\frac{t_{n}}{Theta}\right)\right)\right] + \left(\frac{n}{Beta}\right) - (n \cdot Kappa \cdot \ln(Theta)) + \left(\sum_{j=1}^{n} \ln(t_{j})\right) + \left[(Kappa - 1) \cdot \left[\sum_{k=1}^{n} \frac{\left[\left(t_{k}\right)^{Beta} \cdot \ln(t_{k})\right] - \left[\left(t_{k-1}\right)^{Beta} \cdot \ln(t_{k-1})\right]}{\left[\left(t_{k}\right)^{Beta} - \left(t_{k-1}\right)^{Beta}\right]}\right]\right] = 0$$

$$\frac{\partial l}{\partial \boldsymbol{k}} = (-n \cdot Psi(Kappa)) - (n \cdot Beta \cdot \ln(Theta)) + \sum_{i=1}^{n} \ln\left[\left(t_{i}\right)^{Beta} - \left(t_{i-1}\right)^{Beta}\right] = 0$$

> Here Psi denotes the di-gamma function

$$\mathbf{j}(x) = \frac{\Gamma'(x)}{\Gamma(x)}$$





### Modulated Power Law Process Asymptotic Confidence Intervals

Without pivotal quantities, we must resort to asymptotic confidence intervals for the parameters. The asymptotic distribution of the estimator

$$\left[\hat{q},\hat{b},\hat{k}\right]$$

> Is multivariate normal with mean and covariance

$$\mathbf{m} = [\mathbf{q}, \mathbf{b}, \mathbf{k}] \qquad \sum = [J(\mathbf{q}, \mathbf{b}, \mathbf{k})]^{-1}$$

Where the J matrix is the Jacobian and contains the second partial derivatives of the likelihood function. Approximate confidence intervals for the parameters are given by

$$\widehat{\boldsymbol{q}} \pm z_{\boldsymbol{a}/2} \sqrt{(1,1)entry \left[ J(\widehat{\boldsymbol{q}},\widehat{\boldsymbol{b}},\widehat{\boldsymbol{k}}) \right]^{-1}} \qquad \widehat{\boldsymbol{b}} \pm z_{\boldsymbol{a}/2} \sqrt{(2,2)entry \left[ J(\widehat{\boldsymbol{q}},\widehat{\boldsymbol{b}},\widehat{\boldsymbol{k}}) \right]^{-1}} \qquad \widehat{\boldsymbol{k}} \pm z_{\boldsymbol{a}/2} \sqrt{(3,3)entry \left[ J(\widehat{\boldsymbol{q}},\widehat{\boldsymbol{b}},\widehat{\boldsymbol{k}}) \right]^{-1}}$$

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#### **Modulated Power Law Process**

#### **Simulation Results**

95% Confidence Intervals (no transformation)

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Theta	Beta	Kappa	N	Theta CI %	Beta CI %	Kappa CI %
200	0.75	1	10	77.6	89.7	97.1
200	0.75	1	20	85	93.9	95.8
200	0.75	1	30	86.8	92.9	95.5
200	11	1	10	81.2	92.4	97.6
200	1	11	20	87.1	93.8	96.6
200	1	1	30	89.6	92.9	95.8
200	1.5	1	10	80.2	91	96.7
200	1.5	100	20	90.1	93.7	96.2
200	1.5	1	30	91.5	96.6	95.4
	25/3/	Sirk Co.	1 300	REAL PROPERTY.	1000	All Divine
Theta	Beta	Kappa	N	Theta CI %	Beta CI %	Kappa CI %
200	0.75	2	10	74.8	89.8	98.1
200	0.75	2	20	85.3	92.7	96.3
200	0.75	2	30	85.1	93.1	96.4
200	1	2	10	78.5	88.4	98
200	1	2	20	88	93.3	96
200	1	2	30	90.7	94.1	96.3
200	1.5	2	10	81.8	88	98
200	1.5	2	20	88.7	93	95.7
200	1.5	2	30	90.1	92.2	96.9
Al Some	11	100	155	36 11 W	114	Sale of the
	1878	7.7	100	A. 1. A. 1.		
Theta	Beta	Kappa	N	Theta CI %	Beta CI %	Kappa CI %
200	0.75	3	10	74.7	90.3	97.8
200	0.75	3	20	85	92.1	96.4
200	0.75	3	30	85.5	93.1	95.6
200	-1 1	3	10	80.4	90.1	98.5
200	1	3	20	86.4	91.5	96.9
200	1	3	30	86.9	94.2	96
200	1.5	3	10	81.1	87.4	98
200	1.5	3	20	88.3	91.6	96.3
200	1.5	3	30	89.2	92.3	96.3



### Modulated Power Law Process Asymptotic Confidence Intervals (log transformation - continued)

The approximate confidence intervals are therefore:

q

$$\left[\hat{\boldsymbol{q}} \exp\left\{-z_{\mathbf{a}/2} \sqrt{(1,1) \ entry \ in \left[J(\hat{\boldsymbol{q}}, \hat{\boldsymbol{b}}, \hat{\boldsymbol{k}})\right]^{-1}} / \hat{\boldsymbol{q}}\right\}, \ \hat{\boldsymbol{q}} \exp\left\{z_{\mathbf{a}/2} \sqrt{(1,1) \ entry \ in \left[J(\hat{\boldsymbol{q}}, \hat{\boldsymbol{b}}, \hat{\boldsymbol{k}})\right]^{-1}} / \hat{\boldsymbol{q}}\right\}\right]$$

b

$$\left[\hat{\boldsymbol{b}} \exp\left\{-z_{\boldsymbol{a}/2} \sqrt{(2,2) \ entry \ in \left[J(\hat{\boldsymbol{q}}, \hat{\boldsymbol{b}}, \hat{\boldsymbol{k}})\right]^{-1}}/\hat{\boldsymbol{b}}\right\}, \ \hat{\boldsymbol{b}} \exp\left\{z_{\boldsymbol{a}/2} \sqrt{(2,2) \ entry \ in \left[J(\hat{\boldsymbol{q}}, \hat{\boldsymbol{b}}, \hat{\boldsymbol{k}})\right]^{-1}}/\hat{\boldsymbol{b}}\right\}\right]$$

**k**:

$$\left[ \mathbf{k} \exp \left\{ -z_{\mathbf{a}/2} \sqrt{(3,3) \text{ entry in } \left[ J(\hat{\mathbf{q}}, \hat{\mathbf{b}}, \mathbf{k}) \right]^{-1}} / \mathbf{k} \right\}, \mathbf{k} \exp \left\{ z_{\mathbf{a}/2} \sqrt{(3,3) \text{ entry in } \left[ J(\hat{\mathbf{q}}, \hat{\mathbf{b}}, \mathbf{k}) \right]^{-1}} / \mathbf{k} \right\} \right]$$

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#### **Modulated Power Law Process**

#### **Simulation Results**

95% Confidence Intervals (log transformation)

Theta	Beta	Kappa	N	Theta CI %	Beta CI %	Kappa CI %
200	0.75	1	10	86.3	85.5	85.8
200	0.75	1	20	89.9	89.6	89.7
200	0.75	1	30	91.5	92.5	92.9
200	1	1	10	87.6	88.1	86.2
200	1	1	20	90.9	90.7	92.6
200	1	1	30	90.5	91.5	91
200	1.5	1	10	85.7	87.1	85.8
200	1.5	1	20	91.9	91	91
200	1.5	1	30	91.9	91.8	92.4
VALUE OF THE	150134	State of	36343	THE WORLD	1 Sept 1	A TO MAKE
Theta	Beta	Kappa	N	Theta CI %	Beta CI %	Kappa CI %
200	0.75	2	10	88.7	87.9	85.8
200	0.75	2	20	93	92.3	91.8
200	0.75	2	30	92.5	93.2	91.4
200	1	2	10	88.5	87	87.2
200	1	2	20	93.3	92.4	93
200	1	2	30	93.1	93.2	93.9
200	1.5	2	10	88.6	85.7	84.2
200	1.5	2	20	91.8	90.9	91.5
200	1.5	2	30	92.7	92.6	91.9
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Section 1	25/34	12 May 1	5/3	L. dir No.	1 25/	a director
Theta	Beta	Kappa	N	Theta CI %	Beta CI %	Kappa CI %
200	0.75	3	10	88.1	88.2	85
200	0.75	3	20	91.9	91	91.1
200	0.75	3	30	93.5	92.8	92.6
200	1	3	10	88.4	87.6	86.6
200	1	3	20	91.4	89.7	90.2
200	1	3	30	93.6	93.7	91.8
200	1.5	3	10	88	86.8	84.9
200	1.5	3	20	92.8	91.2	90.7
200	1.5	3	30	92.1	91.6	91.3
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#### **Modulated Power Law Process**

#### **Simulation Results**

Comparison of 95% Confidence Intervals (standard vs. log transformation) that include Kappa = 1

Theta         Beta         Kappa         N         Include Kappa = 1         Include Kappa = 1 (log)           200         0.75         1         10         97.1         85.8           200         0.75         1         20         95.8         89.7           200         0.75         1         30         95.5         92.9           200         1         1         10         97.6         86.2           200         1         1         20         96.6         92.6           200         1         1         30         95.8         91           200         1.5         1         10         96.6         92.6           200         1.5         1         20         96.6         92.6           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.8         39.4           200         1.5         2         10         95.8         39.4           200         0.75         2         30         27.1         9.6 <th></th> <th></th> <th></th> <th></th> <th>The second second second</th> <th>CONTRACTOR OF THE PERSON NAMED IN COLUMN</th>					The second second second	CONTRACTOR OF THE PERSON NAMED IN COLUMN
200         0.75         1         20         95.8         89.7           200         0.75         1         30         95.5         92.9           200         1         1         10         97.6         86.2           200         1         1         20         96.6         92.6           200         1.5         1         10         96.7         85.8           200         1.5         1         20         96.2         91           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         2         20         57.4         22.2           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200	Theta	Beta	Kappa	N	Include Kappa =1	Inlcude Kappa =1 (log)
200         0.75         1         30         95.5         92.9           200         1         1         10         97.6         86.2           200         1         1         20         96.6         92.6           200         1         1         30         95.8         91           200         1.5         1         10         96.7         85.8           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.8         39.4           200         1.5         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         30         28.8         10           200         1.	200	0.75	1	10	97.1	85.8
200         1         1         10         97.6         86.2           200         1         1         20         96.6         92.6           200         1         1         30         95.8         91           200         1.5         1         10         96.7         85.8           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         2         10         95.8         39.4           200         0.75         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.	200	0.75	-1	20	95.8	89.7
200         1         1         20         96.6         92.6           200         1         1         30         95.8         91           200         1.5         1         10         96.7         85.8           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         0.75         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         30         30         9.5           200         1.5	200	0.75	1	30	95.5	92.9
200         1         1         30         95.8         91           200         1.5         1         10         96.7         85.8           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         3         20         11         1.4           200         0.75 </td <td>200</td> <td>1</td> <td>1</td> <td>10</td> <td>97.6</td> <td>86.2</td>	200	1	1	10	97.6	86.2
200         1.5         1         10         96.7         85.8           200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         1.5         1         30         95.4         92.4           200         1.5         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0	200	1	1	20	96.6	92.6
200         1.5         1         20         96.2         91           200         1.5         1         30         95.4         92.4           200         0.75         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         1.5         2         30         30         9.5           200         1.5         3         10         87.2         11.2           200         0.75         3         30         0.7         0.1           200         1 <td>200</td> <td>1</td> <td>1</td> <td>30</td> <td>95.8</td> <td>91</td>	200	1	1	30	95.8	91
200       1.5       1       30       95.4       92.4         200       0.75       2       10       95.8       39.4         200       0.75       2       20       57.4       22.2         200       0.75       2       30       27.1       9.6         200       1       2       10       97.5       42         200       1       2       20       60.9       21         200       1       2       30       28.8       10         200       1.5       2       10       95.2       40.2         200       1.5       2       10       95.2       40.2         200       1.5       2       20       57.6       20.5         200       1.5       2       30       30       9.5         200       1.5       2       30       30       9.5         200       0.75       3       10       87.2       11.2         200       0.75       3       30       0.7       0.1         200       1       3       10       87.3       10.7         200       1       3	200	1.5	1 1	10	96.7	85.8
200         0.75         2         10         95.8         39.4           200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         1.5         2         30         30         9.5           200         1.5         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1	200	1.5	1	20	96.2	91
200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         20         11.8         1           200         1.5	200	1.5	1	30	95.4	92.4
200         0.75         2         20         57.4         22.2           200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         20         11.8         1           200         1.5	3000	575	10 Car 3	ALCOHOLD BY	The state of the	THE RESIDENCE OF
200         0.75         2         30         27.1         9.6           200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1.5	200	0.75	2	10	95.8	39.4
200         1         2         10         97.5         42           200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1         3         30         0.8         0           200         1.5         3	200	0.75	2	20	57.4	22.2
200         1         2         20         60.9         21           200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1.5         3         10         86.6         12.1           200         1.5         3         20         11.2         0.8	200	0.75	2	30	27.1	9.6
200         1         2         30         28.8         10           200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1.5         3         10         86.6         12.1           200         1.5         3         20         11.2         0.8	200	1.	2	10	97.5	42
200         1.5         2         10         95.2         40.2           200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1         3         30         0.8         0           200         1.5         3         10         86.6         12.1           200         1.5         3         20         11.2         0.8	200	1	2	20	60.9	21
200         1.5         2         20         57.6         20.5           200         1.5         2         30         30         9.5           200         0.75         3         10         87.2         11.2           200         0.75         3         20         11         1.4           200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1         3         30         0.8         0           200         1.5         3         10         86.6         12.1           200         1.5         3         20         11.2         0.8	200	1	2	30	28.8	10
200     1.5     2     30     30     9.5       200     0.75     3     10     87.2     11.2       200     0.75     3     20     11     1.4       200     0.75     3     30     0.7     0.1       200     1     3     10     87.3     10.7       200     1     3     20     11.8     1       200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	1.5	2	10	95.2	40.2
200     0.75     3     10     87.2     11.2       200     0.75     3     20     11     1.4       200     0.75     3     30     0.7     0.1       200     1     3     10     87.3     10.7       200     1     3     20     11.8     1       200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	1.5	2	20	57.6	20.5
200     0.75     3     20     11     1.4       200     0.75     3     30     0.7     0.1       200     1     3     10     87.3     10.7       200     1     3     20     11.8     1       200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	1.5	2	30	30	9.5
200     0.75     3     20     11     1.4       200     0.75     3     30     0.7     0.1       200     1     3     10     87.3     10.7       200     1     3     20     11.8     1       200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	The same		St. Ach.	1 16	THE WAY TO	
200         0.75         3         30         0.7         0.1           200         1         3         10         87.3         10.7           200         1         3         20         11.8         1           200         1         3         30         0.8         0           200         1.5         3         10         86.6         12.1           200         1.5         3         20         11.2         0.8	200	0.75	3	10	87.2	11.2
200     1     3     10     87.3     10.7       200     1     3     20     11.8     1       200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	0.75	3	20	11	1.4
200     1     3     20     11.8     1       200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	0.75	3	30	0.7	0.1
200     1     3     30     0.8     0       200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	1	3	10	87.3	10.7
200     1.5     3     10     86.6     12.1       200     1.5     3     20     11.2     0.8	200	1	3	20	11.8	1
200 1.5 3 20 11.2 0.8	200	1	3	30	0.8	0
	200	1.5	3	10	86.6	12.1
200 1.5 3 30 0.4 0.1	200	1.5	3	20	11.2	0.8
	200	1.5	3	30	0.4	0.1



## Modulated Power Law Process Hypothesis Testing

Previously we discussed the special cases of the MPLP. This leads to the following tests of hypothesis

 $H_0: \mathbf{k} = 1$ , versus  $H_1: \mathbf{k} \neq 1$  (model reduces to the Power Law Process)

 $H_0: \mathbf{k} = 1$ , versus  $H_1: \mathbf{k} \neq 1$  (model reduces to Gamma renewal process)

 $H_0: \mathbf{k} = 1$ ,  $versus\ H_1: \mathbf{k} \neq 1$  (model reduces to homogeneous Poisson Process)

> Since the exact distributions of the estimators are intractable, we rely on asymptotic results. The likelihood ratio test statistic is given by

$$LR = \frac{\max_{(\boldsymbol{q},\boldsymbol{b},\boldsymbol{k}) \in S} L(\boldsymbol{q},\boldsymbol{b},\boldsymbol{k})}{\max_{(\boldsymbol{q},\boldsymbol{b},\boldsymbol{k})} L(\boldsymbol{q},\boldsymbol{b},\boldsymbol{k})}$$



# Modulated Power Law Process Hypothesis Testing (continued)

> Test I:  $H_0$ : k=1 If the Null hypothesis is true, then the failure process is a power law process with parameters q, b.

$$LR_{PLP} = \frac{\max_{(q,b,k) \in S} L(\widehat{q}_{PLP}, \widehat{b}_{PLP}, 1)}{\max_{(q,b,k)} L(\widehat{q}, \widehat{b}, \widehat{k})}$$

Where 
$$\widehat{m{b}}_{PLP} = rac{n}{\displaystyle\sum_{i=1}^{n-1} \log rac{t_n}{t_i}}$$
 and  $\widehat{m{q}} = rac{t_n}{\displaystyle\frac{1}{n}}$ 

> Reject 
$$H_0: \mathbf{k} = 1$$
 if  $-2 \log LR_{PLP} > c_{1-a}^2(1)$ 



# Modulated Power Law Process Hypothesis Testing (continued)

> Test II:  $H_0: k=1$  If the Null hypothesis is true, then the failure process is a gamma renewal (times between failures are iid random variables) M(k,q)

$$LR_{GRP} = \frac{\max_{(\boldsymbol{q}, \boldsymbol{b}, \boldsymbol{k}) \in S} L(\widehat{\boldsymbol{q}}_{GRP}, 1, \widehat{\boldsymbol{k}}_{GRP})}{\max_{(\boldsymbol{q}, \boldsymbol{b}, \boldsymbol{k})} L(\widehat{\boldsymbol{q}}, \widehat{\boldsymbol{b}}, \widehat{\boldsymbol{k}})}$$

> The MLEs of theta and kappa do not have a closed form expression and must be solved by numerical methods. Differentiating the likelihood function and setting the results equal to zero leads to

$$\widehat{\mathbf{q}} = \frac{\overline{x}}{\widehat{\mathbf{k}}} \qquad \log \mathbf{k} - \frac{\Gamma'(\mathbf{k})}{\Gamma(\mathbf{k})} - \log(\overline{x}/\widetilde{x}) \qquad \widetilde{x} = (\prod x_i)^{1/n}$$

> Reject 
$$H_0: \mathbf{b} = 1$$
 if  $-2 \log LR_{GRP} > \mathbf{c}_{1-\mathbf{a}}^2(1)$ 



# Modulated Power Law Process Hypothesis Testing (continued)

Test III:  $H_0$ :  $\mathbf{b} = \mathbf{k} = 1$  If the Null hypothesis is true, then the failure process is a homogeneous Poisson process (times between failures are iid EXP(q) random variables).

$$LR_{HPP} = \frac{\max_{(q,b,k) \in S} L(\widehat{q}_{HPP},1,1)}{\max_{(q,b,k)} L(\widehat{q},\widehat{b},k)}$$

$$\rightarrow$$
 Where  $\hat{q}_{HPP} = \frac{t_n}{n}$ 

> Reject 
$$H_0: \mathbf{b} = \mathbf{k} = 1$$
 if  $-2 \log LR_{GRP} > c_{1-a}^2(2)$ 





## Modulated Power Law Process Simulation Results – Hypothesis Testing

**TEST:**  $H_0: b = 1$   $H_a: b \ne 1$ 

N	Theta	Beta	Kappa	Reject Ho
20	200	1	3	6.00%
20	200	1.25	3	45.70%
20	200	1.5	3	88.60%
20	200	2	3	99%

N	Theta	Beta	Kappa	Reject Ho
30	200	150	3	5.90%
30	200	1.25	3	67.30%
30	200	1.5	3	97.40%
30	200	2	3	98.4%

Results of hypothesis test on Beta with alpha = .05





## Modulated Power Law Process Simulation Results – Hypothesis Testing

**TEST:**  $H_0: k = 1$   $H_a: k \neq 1$ 

N	Theta	Beta	Kappa	Reject Ho
20	200	1.5	1	6.00%
20	200	1.5	1.5	34.70%
20	200	1.5	2	71.70%
20	200	1.5	2.5	90.8%
20	200	1.5	3	98.4%
20	200	1.5	4	100%

N	Theta	Beta	Kappa	Reject Ho
30	200	1.5	1	5.70%
30	200	1.5	1.5	45.93%
30	200	1.5	2	86.90%
30	200	1.5	2.5	98.9%
30	200	1.5	3	100.0%
30	200	1.5	4	100.0%

Results of hypothesis test on Kappa with alpha = .05





## Modulated Power Law Process Mission Readiness

> From the definition of the Inhomogeneous Gamma Process

$$f(t_1, t_2, \dots, t_n) = \left\{ \prod_{i=1}^{n} \boldsymbol{I}(t_i) \left[ \Lambda(t_i) - \Lambda(t_{i-1}) \right]^{K-1} \right\} \frac{\exp(-\Lambda(t_i))}{\Gamma(K)^n}$$

where 
$$\Lambda(t) = \int_{0}^{t} \mathbf{I}(t)dt$$
 and  $\mathbf{I}(t) = \left(\frac{\mathbf{b}}{\mathbf{q}}\right)\left(\frac{t}{\mathbf{q}}\right)^{\mathbf{b}-1}$ 

> READINESS: Probability of no failures P( N=0) in a specified mission time given the current state of the system (conditional probability density function).

$$f_n(t_n/t_{n-1}) = \lim_{\Delta t \to 0} \Pr(t < T_n < t + \Delta t / T_{n-1} = t)$$



# Modulated Power Law Process Mission Readiness (continued)

Using the intensity function for the PLP

$$f_{n}(t/t_{n-1}) = \frac{\left\{\prod_{i=1}^{n} \left(\frac{\boldsymbol{b}}{\boldsymbol{q}}\right) \left(\frac{t_{i}}{\boldsymbol{q}}\right)^{b-1} \left[\left(\frac{t_{i}}{\boldsymbol{q}}\right)^{b} - \left(\frac{t_{i-1}}{\boldsymbol{q}}\right)^{b}\right]^{k-1}\right\} \frac{\exp\left(-\left(\frac{t_{n}}{\boldsymbol{q}}\right)^{b}\right)}{\Gamma(\boldsymbol{k})^{n}}}{\left\{\prod_{i=1}^{n-1} \left(\frac{\boldsymbol{b}}{\boldsymbol{q}}\right) \left(\frac{t_{i}}{\boldsymbol{q}}\right)^{b-1} \left[\left(\frac{t_{i}}{\boldsymbol{q}}\right)^{b} - \left(\frac{t_{i-1}}{\boldsymbol{q}}\right)^{b}\right]^{k-1}\right\} \frac{\exp\left(-\left(\frac{t_{n-1}}{\boldsymbol{q}}\right)^{b}\right)}{\Gamma(\boldsymbol{k})^{n-1}}}$$

> Which reduces to

$$f_n(t_n/t_{n-1}) = \frac{bt_n^{b-1}}{\Gamma(k)q^b} \left[ \left( \frac{t_n}{q} \right)^b - \left( \frac{t_{n-1}}{q} \right)^b \right]^{k-1} \exp \left\{ - \left[ \left( \frac{t_n}{q} \right)^b - \left( \frac{t_{n-1}}{q} \right)^b \right] \right\}$$



# Modulated Power Law Process Mission Readiness (continued)

> If we define

$$a(t_n) = \left(\frac{t_n}{\boldsymbol{q}}\right)^b - \left(\frac{t_{n-1}}{\boldsymbol{q}}\right)^b$$

> then

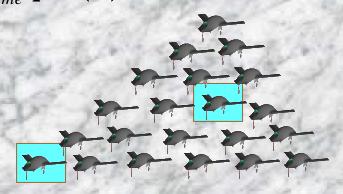
$$f(t_n/t_{n-1}) = \frac{\boldsymbol{b}}{\boldsymbol{q}^{\boldsymbol{b}} \Gamma(\boldsymbol{k})} t_n^{\boldsymbol{b}-1} a(t_n)^{\boldsymbol{k}-1} \exp(-a(t_n))$$



# Modulated Power Law Process Mission Readiness (continued)

> The probability of no failures in a given mission time is given by

$$\int_{\text{Mission EndTime}}^{\infty} \frac{\boldsymbol{b}}{\boldsymbol{q}^{b} \Gamma(\boldsymbol{k})} t_{n}^{b-1} a(t_{n})^{k-1} \exp(-a(t_{n})) dt_{n}$$



> Select required aircraft with highest probability of mission completion



### Summary

- Modulated Power Law Process provides ability to model improvement into repairable systems.
- Inference procedures capable of detecting special cases.
- Asymptotic confidence intervals were very effective in simulation study (nominal level) for sample size > 30.
- Conditional distribution presented Estimating probability of failure in a given mission time (readiness).
- Modulated Power Law Process provides insight into the overall support process. Kappa can be used as support improvement measure.